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# CURRENT VOLTAGE CHARACTERISTICS OF SEMICONDUCTOR HETEROSTRUCTURES – INTEGRATION OF SHARPLY PEAKED TRANSMISSIVITIES

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Abstract: We investigate the current through a multibarrier/quantum well heterostructure assuming conservation of energy and of the momentum parallel to the interfaces. This current is given by the Esaki integral over the transmissivity  $T(E, V_a)$ . Energies with T(E,0) = 1 correspond to the eigenvalues of the structure. For an applied voltage  $V_a$  the maxima give the resonances of the structure, whose widths are a measure for the tunneling probability through the corresponding barriers. If these probabilities are small, then the resonance lines become extremely narrow. If the precision of the computation is only a few orders of magnitude smaller, the results are very sensitive to the integration method especially near the first maximum of the  $J(V_a)$  characteristic. Here we consider an extension of the trapezoidal method, which includes an exponential grid pattern near the resonances, taking into account the strong variation of  $T(E, V_a)$ . A few examples of simple heterostructure characteristics will be discussed.

Tunneling in heterostructures [1] consisting of AlGaAs barriers (width  $b_1, b_2$ ; height  $V_1, V_2$ ) separated by a well of GaAs (width  $b_{12}$ ; height  $V_{12} = 0$ ) is the subject of intensive investigation. In the present work current-voltage characteristics derived from a simplified theory (ideal interfaces, no lateral inhomogeneities, no coherence-destroying effects such as inelastic scattering) resulting in the Esaki formula [2] are evaluated numerically. Comparison with the systematic experimental study by Guéret *et al.* will be published elsewhere [3],[4].

Consider independent quasifree electrons moving in an electric field  $V_a/L_a$  ( $L_a$  is the total length of the junction with a voltage  $V_a$  applied). Summed over the transverse *k*-vectors, the total current density as an integral over the longitudinal energies becomes

$$J(V_a) = \frac{em_l\theta}{2\pi\hbar^3} \int dET(E, V_a) \ln \frac{1 + \exp(E_F - E)/\theta}{1 + \exp(E_F - E - V_a)/\theta}$$

where applied voltage  $V_a$  and temperature  $\theta = k_B T_K$  are measured in energy units (eV).  $T(E,V_a)$  is the transmissivity of the structure, i.e. the portion of electrons transmitted, which together with the reflectivity R adds up to T + R = 1. T can be found by the exact Airy-function [5] solution, whose coefficients related through four transfer matrices define T. Because of the lack of polynomial representations of Ai and Bi a plane wave approximation in subslices of width w ( $w \sim 10$  Å) is used here, assuming a constant potential in each subslice.

For our typical symmetric double barrier junctions  $b_1 = b_2 = 275$  Å,  $V_1 = V_2 = 0.12$  eV,  $b_{12} = 70$  Å,  $E_F = 0.012$  eV and  $T_K = 4.2^\circ$ , the transmissivity exhibits resonance peaks at energies  $E_r(V_a)$ , which for small  $V_a$  are narrow and well separated. The shape is Gaussian for  $|E - E_r| \le \Delta E_r^l$  and like  $1/(E - E_r)^2$  (Lorentzian) for  $|E - E_r| \gg \Delta E_r^l$  ( $\Delta E_r^l$  is the halfwidth of the r-th resonance) as long as the next resonance is not interfering. With increasing  $V_a$ , resonances shift towards smaller energies  $E_r(V_a) = E_{r0} - 0.5V_a + O(V_a^2)$  and increase in width according to  $\Delta E'_r(V_a) = \Delta E_{r0}(1 + C_r V_a^2 + ...)$ ; values for the above parameters are  $\Delta E_{10} = 5.2 \times 10^{-11} \text{ eV}$ , (C<sub>1</sub> = 850),  $\Delta E'_{20} = 1.7 \times 10^{-4}$ , etc. Because of the extremely small width of the first resonance, which contributes mainly to the first maximum in the  $J(V_a)$ characteristic, a special integration method has been developed. It is an extension of the trapezoidal method [6] by means of linearly distributed grid points with grid interval  $\delta E$ including an r-dependent exponential grid near resonance energies according to  $E_{r\lambda}^{\pm} = E_r(V_a) \pm \delta E_r p_r^{\lambda}$  with  $r = 1, 2, \dots, \lambda = 0, 1, \dots, \Lambda_r$ , where  $\Lambda_r$  is chosen such that  $\delta E_r p_r^{\Lambda_r} \cong \Delta E_r^{I}$ ; because of the exponential decay of the peak,  $p_r \simeq 1/2$  and  $\delta E_r \simeq \delta E$  give best results. The precision has been checked by halving the grid steps, which are typically 10<sup>-3</sup> for our example. Characteristics thus derived are reliable if the subslice width is w = 5 Å if the applied voltages are not too large  $|V_a| < 0.2 \text{ eV}$ .

In contrast to adaptive integration methods [6] our method avoids IF commands and is hence more appropriate for vector processor computing.

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