

Zeitschrift: IABSE reports = Rapports AIPC = IVBH Berichte
Band: 999 (1997)

Artikel: Dynamic response of curved composite cellular bridges
Autor: Sennah, Khaled M. / Kennedy, John B.
DOI: <https://doi.org/10.5169/seals-1107>

Nutzungsbedingungen

Die ETH-Bibliothek ist die Anbieterin der digitalisierten Zeitschriften. Sie besitzt keine Urheberrechte an den Zeitschriften und ist nicht verantwortlich für deren Inhalte. Die Rechte liegen in der Regel bei den Herausgebern beziehungsweise den externen Rechteinhabern. [Siehe Rechtliche Hinweise.](#)

Conditions d'utilisation

L'ETH Library est le fournisseur des revues numérisées. Elle ne détient aucun droit d'auteur sur les revues et n'est pas responsable de leur contenu. En règle générale, les droits sont détenus par les éditeurs ou les détenteurs de droits externes. [Voir Informations légales.](#)

Terms of use

The ETH Library is the provider of the digitised journals. It does not own any copyrights to the journals and is not responsible for their content. The rights usually lie with the publishers or the external rights holders. [See Legal notice.](#)

Download PDF: 21.05.2025

ETH-Bibliothek Zürich, E-Periodica, <https://www.e-periodica.ch>

Dynamic Response of Curved Composite Cellular Bridges

Khaled M. SENNAH

Teaching and Research Assistant
University of Windsor
Windsor, Ontario, Canada

Khaled M. Sennah, born 1962, received his civil engineering degree at Alexandria University, Egypt. Presently carrying out research on static and dynamic responses of curved composite bridges.

John B. KENNEDY

University Distinguished Professor
University of Windsor
Windsor, Ontario, Canada

John B. Kennedy, born 1932, received his engineering degree at University of Wales, U. K. His field of research has been on skew and curved composite bridges as well as soil-metal structures.

Summary

This paper is a summary of an extensive parametric study, using the finite-element method, in which 120 simply-supported curved composite bridge prototypes are analyzed to evaluate their natural frequencies and mode shapes. The parameters considered in the study are: end-diaphragm thickness, cross-bracing system, degree of curvature, and number of cells. Results from tests on four 1/12 linear-scale simply-supported composite three-cell bridge models of different curvatures are used to substantiate the analytical modelling.

1-Results and conclusion

Dynamic analysis of simply-supported curved multi-cell composite bridges was conducted using the finite-element modelling. This modelling was verified by results from free-vibration testing of four simply-supported composite three-cell bridge models. Figure 1 shows the cross-sectional details of the models. Two diaphragms, 5 mm thick, were placed radially at the extreme end sections. No inner bracings were used in the second model while in the other models, five cross-bracings of rectangular cross-section 13×5 mm were installed in the radial direction, at equal intervals. The span-to-radius ratios were 1.0 in both the first and second models, 0.375 in the third model, and 0.0 in the fourth model. Table 1 summarizes the natural frequencies and mode shapes of the bridge models. Good agreement between the experimental and theoretical findings can be observed. It is observed that the dominant mode of vibration of a curved bridge is a combined flexural and torsional mode, with the bridge frequency decreasing with an increase in the degree of curvature. Also, the presence of cross-bracings enhances the first two natural frequencies in the first model when compared to those in the second model. Figure 2 presents the effect of end-diaphragm thickness on the dominant frequency. It is observed that the presence of end-diaphragms enhances the dominant frequency and its mode shapes. Figure 3 shows that for curved bridges, a minimum of three cross-bracings are adequate to enhance the dominant frequency due to increased torsional resistance. Figure 4 shows that the dominant frequency decreases with increase in the curved span as well as in the degree of curvature. In the case of one- and two-lane bridges, when the number of cells is ≤ 3 , increasing the number of cells increases the dominant frequency as shown in Figure 5. In the case of bridges with any number of lanes and with number of cells ≥ 3 , the change in the number of cells has no significant effect on the dominant frequency. Expressions for the first flexural frequency and hence the dynamic load allowance for this type of bridges has also been deduced and reported elsewhere*.

* Sennah, K. M. 1997. Static and dynamic responses of curved composite concrete deck-steel multi-cell bridges. Ph.D dissertation, University of Windsor, Windsor, Ontario, Canada.

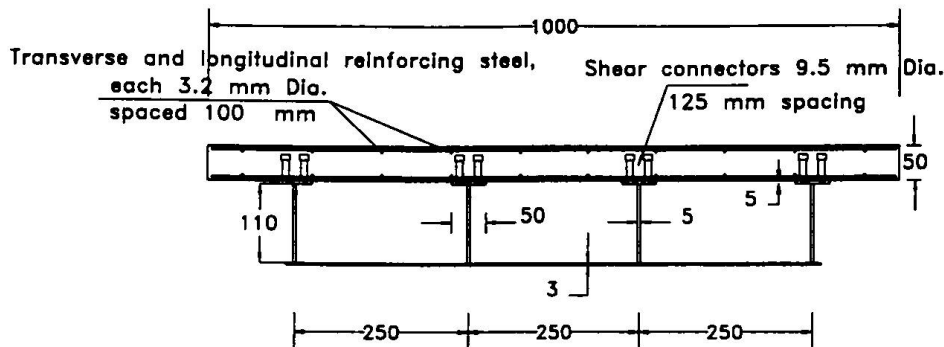


Fig. 1. Cross-sectional details of models

Model No.	L (m)	$\frac{L}{R}$	First natural frequency (Hz)			Second natural frequency (Hz)		
			Experimental	Finite-element	Mode shape	Experimental	Finite-element	Mode shape
1	2.6	1	38	39	LF-TS	125	133	TS
2	2.6	1	36	38	LF-TS	81	91	TS
3	2.6	0.375	44	46	LF-TS	-	138	TS
4	2.6	∞	45	47	LF	-	136	TS

Note: LF: Longitudinal flexure; TS: Symmetric Torsion

Table 1. Natural frequencies and mode shapes of tested bridge models

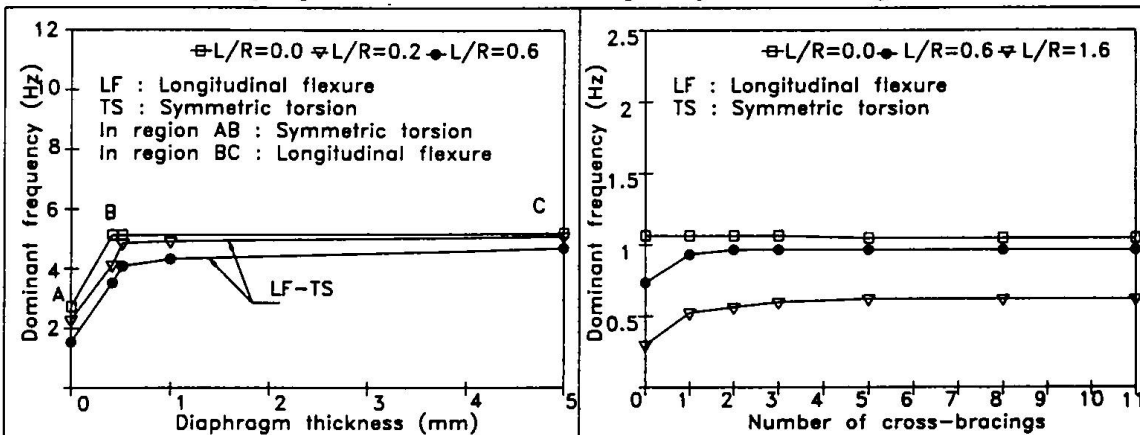


Fig. 2. Effect of end-diaphragm thickness on the dominant frequency of three-lane five-cell bridges

Fig. 3. Effect of cross-bracings on the dominant frequency of two-lane three-cell bridges of span = 100 m

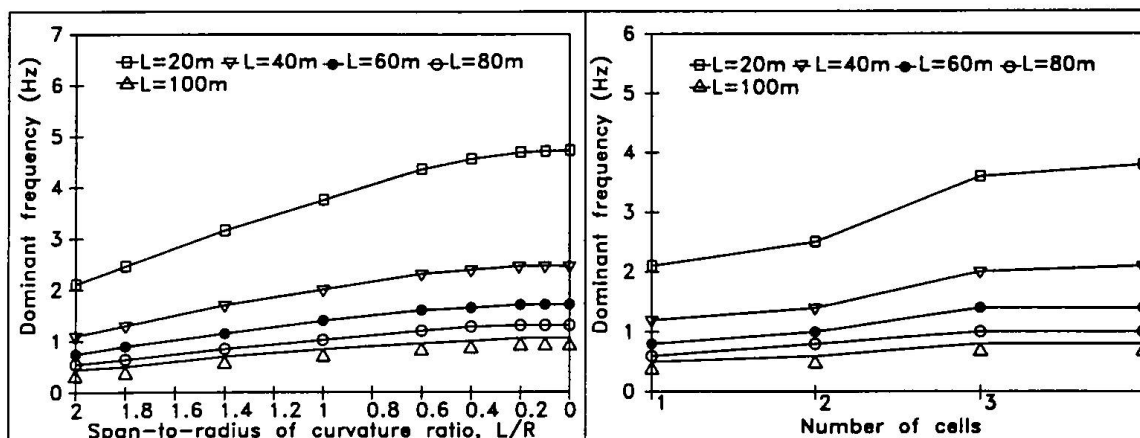


Fig. 4. Effect of curvature on the dominant frequency of two-lane three-cell bridges

Fig. 5. Effect of number of cells on the dominant frequency of two-lane three-cell bridges with $L/R=1.0$