

**Zeitschrift:** IABSE reports = Rapports AIPC = IVBH Berichte  
**Band:** 73/1/73/2 (1995)  
  
**Artikel:** New approach in the ultimate life calculation for cracked concrete  
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**DOI:** <https://doi.org/10.5169/seals-55343>

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## **New Approach in the Ultimate Life Calculation for Cracked Concrete**

Nouvelle méthode d'évaluation de la durée de service de structures  
en béton armé

Eine neue Methode zur Bemessung von Stahlbetonkonstruktionen  
im gerissenen Zustand

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### **SUMMARY**

The paper describes a new proposal for the design of reinforced concrete structures in an aggressive environment. The procedure takes into account the real condition of concrete section cracking under dead and live loads and special durable loads. In this way the least possible probability of structural damage resulting from the effect of special durable loads, can be provided for already in the design phase.

### **RÉSUMÉ**

L'article propose une nouvelle méthode pour le projet de constructions en béton armé dans un environnement agressif. La procédure prend en compte l'état réel de la fissuration du béton sous charges permanentes et variables et sous charges spéciales durables. Cette méthode permet de prévoir, déjà lors de l'établissement du projet, les dommages structuraux les moins probables qui proviennent de l'effet de charges spéciales durables.

### **ZUSAMMENFASSUNG**

Eine neue Methode zur Bemessung von Stahlbetonkonstruktionen in aggressiver Umgebung wird beschrieben. Das Verfahren zieht in Betracht reelle Verhältnisse von Stahlbetonquerschnitten im gerissenen Zustand unter ständigen Verkehrslasten und speziellen Dauerlasten (Umgebungseinflüssen). Die kleinstmögliche Wahrscheinlichkeit von strukturellen Schäden kann so schon in der Projektphase gesichert werden.



## 1. INTRODUCTION

The fulfillment of the crack limitation criteria frequently results in considerable increase of reinforcement necessary for ultimate limit state design, as well as other criteria of serviceability limit state. However, the manifestation of cracks greater than obtained by the calculations and prescribed, cannot be completely eliminated. Therefore, this paper proposes to introduce the new criterion of the serviceability limit state instead of the cracking limit state. In this way, other numerous factors of reinforced structure durability could be considered.

Such additional durability factors are proposed to be called "special durable loads" [1]. As special durable loads increase material degradation, especially reinforcement corrosion, the new criterion is proposed to be called "the criterion of corrosion limit state" [1].

According to the corrosion limit state it is necessary to prove that the calculated service life  $t_c$  is higher or at least equal to the designed life  $t_p$ :

$$t_0 + t_1 = t_c > t_p \quad /1/$$

where:

$t_0$  is period of initiation of reinforcement corrosion in concrete,

$t_1$  is period of propagation of reinforcement corrosion in concrete [2].

## 2. PERIOD OF INITIATION AND PERIOD OF PROPAGATION REINFORCEMENT CORROSION PROCESS IN CONCRETE

The period of initiation of reinforcement corrosion in concrete stimulated by chlorides (structures in marine environment or structures on roads where the surfaces are strewn with salt for defrosting in the conditions of continental winters), can be determined by diffusion analysis of chlor ions in reinforced concrete cross-sections. The time necessary for the concentration of chlor ions to reach the critical value  $C_{cr}$  on the level of reinforcement should be calculated as follows:

$$C(c, t_0) = C_{cr} = 0.4\% \quad [3] . \quad /2/$$

The continuous diffusion process of chlor ions for time-varying diffusion coefficients and the initial concentration of chlor ions is most appropriately expressed by the following experimental formula [1]:

$$C(x, t) = \left[ C_0 + k(t - 1) \right] \left( 1 - \operatorname{erf} \frac{x}{2\sqrt{\tau}} \right) + k \left[ \left( 1 + \frac{x^2}{2\tau_1} \right) \left( 1 - \operatorname{erf} \frac{x}{2\sqrt{\tau_1}} \right) - \frac{x}{\sqrt{\pi \cdot \tau_1}} e^{-\frac{x^2}{4\tau_1}} \right], \quad 0 \leq C_0 \leq C_{\max}, \quad /3/$$

while after reaching the maximum starting concentration  $C_0 = C_{\max}$  the following expression is valid:

$$C(x, t) = C_0 \left( 1 - \operatorname{erf} \frac{x}{2\sqrt{\tau}} \right), \quad C_0 = C_{\max} \quad /4/$$

where:

$C_0$  is initial concentration of chlor ions,

$C_{\max}$  is maximum concentration of chlor ions [1, 4],

$k$  is the coefficient of linear increase of initial concentration [1, 5],

$\tau$  is the substitution by which variation of  $D_{Cl}$  with time [4] is being taken into account,

$\tau_1 = \tau(t = 1)$ .

As the structure is located in the aggressive marine environment and as the owner prescribed the life of 100 years, the crack width in concrete is limited to 0.1 mm. The calculations, taking into consideration the criteria of limit cracking condition, resulted in almost 100% increase of reinforcement quantity, compared to the required one from the ultimate limit state design:  $A_s$  ( $w \leq 0.1$  mm) = 14.0 cm<sup>2</sup>/m'.



In order to avoid such an increase, the cross-section will be designed according to the corrosion limit state criterion, which permits the real concrete cracking under the dead and live loads only. Due to marine environment, chlorides can be taken as special durable loads so that the period of corrosion initiation is calculated by the analysis of chlor ions diffusion process (formula /3/ and /4/) and under the following assumptions:

- $w/c = 0.45$ ,
  - $c = 5.0$  cm,
  - $C_0(t=0) = 0$ ,
  - $k = 0.2$  for structures at 50 - 250 m from the sea [1],
  - $C_{max} = 7.64\%$  [4],
  - cement with slag addition,  $D_{01} = 0.3$  [1],
  - crack width  $w = 0.26$  mm,  $D_{02} = 1.08$  [1],  $D_0 = D_{01} \cdot D_{02} = 0.324$  [1],
- and  $t_0 = 17$  years (Fig. 2).

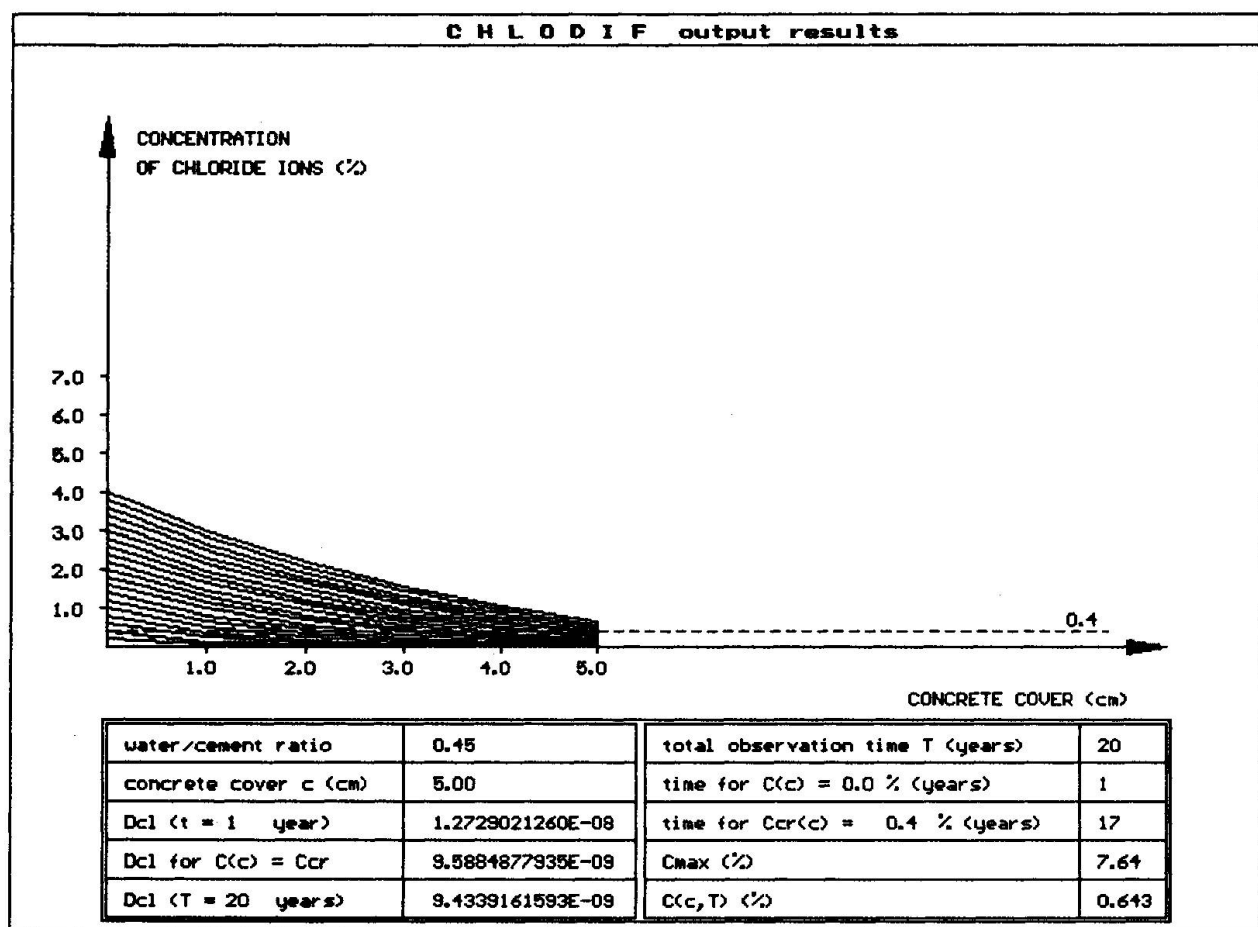


Fig. 2. Analysis of chlor ions diffusion process to the period  $t_0$

The period of corrosion progress, propagation time  $t_1$  with parameters [1]:

$i_{corr} = 0.5 \mu A/cm^2$ ,  $p = 2.37$ ,  $\gamma = 1.2$ , according to the formula /6/ is  $t = 36.7$  years. Calculated life of the arch element is than  $t_c = 17 + 36.7 = 53.7$  years, which is far less than prescribed  $t_p = 100$  years.

The problem is solved in such a way that the necessary value of the initial diffusion coefficient  $D_{Cl} = 2.34 \cdot 10^{-9} cm^2/s$  (prior  $D_{Cl} = 1.27 \cdot 10^{-8} cm^2/s$ , Fig. 2), is read from the nomogram (Fig. 3.) [4, 1], elaborated for the concrete cover thickness  $c = 5$  cm and prescribed period  $t_0 = 64$  years.

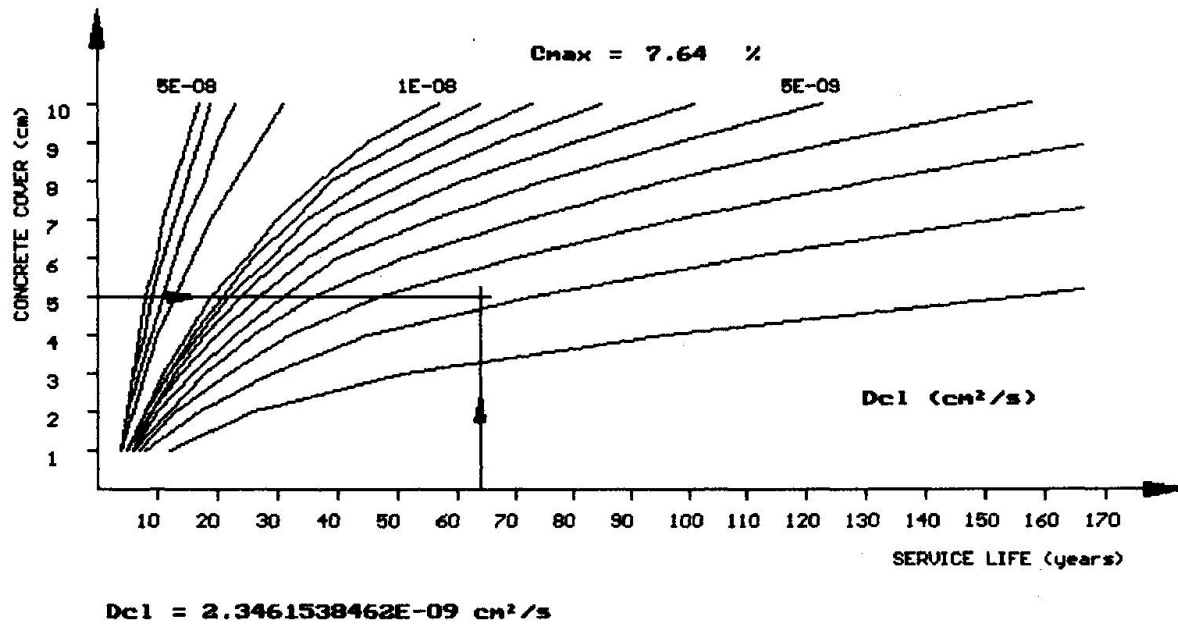


Fig. 3. C-D-c-t nomogram

As it is impossible to fulfill the criteria of the service life of 100 years [8] by above mentioned procedures (the only one remained possibility [8] of water-cement ratio reduction at  $w/c = 0.4$  decreases value of the diffusion coefficient to  $D_{C1} = 8.08 \cdot 10^{-9}$  [1]), it is proposed to apply the mobile corrosion inhibitors [9, 10] in the form of admixtures during concreting or in the form of surface coats, which will in their activation time stop the corrosion process (Table 1, [1]).

t (years)	ACTIVITY
0	Finishing of construction (structural element)
21	Applying of mobile corrosion inhibitors in the form of surface coats
37	Activation of corrosion inhibitors
39	Reaching of critical chlorine ion concentration on reinforcement
64	Stopping of corrosion inhibitors activity, starting of corrosion process
100	Fulfillment of the criterion of corrosion limit state

Table 1 Time schedule of structure maintenance

#### 4. CONCLUSION

The proposed new method is based on supplementing the existing design procedure according cracking limit state design with corrosion limit state design under the conditions of simultaneous action of dead and live loads and special durable loads.

Dimensioning to the corrosion limit state design yields initiation and propagation time for reinforcement corrosion process. This procedure, applied in design phase, frequently results in less reinforcement steel than obtained from standard cracking limit state calculation.



### Acknowledgment

The authors wish to acknowledge Mr Zlatko Šavor for useful advices during the preparation of this paper.

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