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**G**

**MISCELLANEOUS**

**VERSCHIEDENES**

**DIVERS**

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## I. Conversion Table from British to Metric Units.

Length:	1 inch.	=	2.5399978 cm
	1 foot	=	0.3047997 m
	1 yard	=	0.9143992 m
Area:	1 sq. in	=	6.451589 cm <sup>2</sup>
	1 sq. ft.	=	0.092903 m <sup>2</sup>
	1 sq. yd.	=	0.836126 m <sup>2</sup>
Volume:	1 cu. in.	=	16.387021 cm <sup>3</sup>
	1 cu. ft.	=	0.028317 m <sup>3</sup>
	1 cu. yd.	=	0.764553 m <sup>3</sup>
Force:	1 lb.	=	0.453592 kg
	1 kip (1000 lb.)	=	0.453592 t
	1 (long) ton	=	1.016047 t
Stress:	1 lb/sq. in.	=	0.070307 kg/cm <sup>2</sup>
	1 lb/sq. ft.	=	4.882437 kg/m <sup>2</sup>
	1 ton/sq. in.	=	157.4879 kg/cm <sup>2</sup>
Temperature:	$t^{\circ}\text{C} = \frac{t^{\circ}\text{F} - 32}{1.8}$ .		

## II. Conversion Table from Metric to British Units.

Length:	1 cm	=	0.3937011 in.
	1 m	=	3.2808430 ft.
		=	1.0936143 yd.
Area:	1 cm <sup>2</sup>	=	0.155001 sq. in.
	1 m <sup>2</sup>	=	10.763931 sq. ft.
		=	1.195992 sq. yd.
Volume:	1 cm <sup>3</sup>	=	0.061024 cu. in.
	1 m <sup>3</sup>	=	35.314767 cu. ft.
		=	1.307954 cu. yd.
Force:	1 kg	=	2.204622 lb.
	1 t	=	2.204622 kips
		=	0.984206 longton
Stress:	1 kg/cm <sup>2</sup>	=	14.223315 lb/sq. in.
	1 t/cm <sup>2</sup>	=	6.349693 ton/sq. in.
Temperature:	$t^{\circ}\text{F} = 1.8 t^{\circ}\text{C} + 32$ .		

### III. Errata of the "Preliminary Publication".

The "Preliminary Publication" is to be corrected as follows:

#### I 1 A. Freudenthal.

$$\text{p. 7: } \sqrt{\left(\frac{\sigma_x + \sigma_y}{2}\right)^2 + \tau^2} + \sin \rho \frac{\sigma_x + \sigma_y}{2} = C$$

#### I 2 J. Fritzsche.

$$\text{p. 23, eq. (2): } \sigma'_F = \sqrt{\frac{2}{1 + \alpha(1 - \beta)}} \cdot \sigma_F$$

$$\text{p. 33, eq. (13): } \dots = \bar{\sigma}_{o\text{ crit}} [1 + \bar{\sigma}_{o\text{ crit}} \dots]$$

#### I 4 E. Melan.

$$\text{p. 60, 9th 1. from the bottom: } 9_{11} + c_1 \dots 9_{1\lambda}$$

$$\text{p. 62, 9th 1.: } \bar{\sigma}_i + c_i \bar{v}_i = \dots$$

$$\text{p. 63, 10th 1. from the bottom: }$$

$$\dots + c_i (2 w_i^{(\varphi)} + \Delta w_i^{(\varphi+1)}) \Delta w_i^{(\varphi+1)}$$

$$\text{p. 63, 6th 1. from the bottom: } z_i^{(\varphi+1)} = e_i^{(\varphi+1)} - \dots$$

#### I 5 E. Kohl.

$$\text{p. 67: } \dots = \frac{34,5 P'_{Gr}}{50,64 + l_z \frac{F_c}{F_z}} \quad \text{for case a}$$

$$\dots = \frac{34,5 P_{Gr}}{60,54 + l_z \frac{F_c}{F_z}} \quad \text{for case b}$$

#### I 6 R. Lévi.

$$\text{p. 81, 11th 1. from the bottom: } n = \frac{PC}{OP} = \dots$$

#### IIb 1 E. Bornemann.

$$\text{p. 183, at the bottom: } \sigma_b = \frac{(\delta - x)}{\left(\frac{E_e}{E_b} + \frac{1}{\mu}\right)} \cdot E_e$$

#### IId 1 F. Baravalle.

p. 322, Fig. 4: Space between the columns 3.90 instead of 5.30

#### IIIa 1 O. Kommerell.

$$\text{p. 366, eq. (5): } = \frac{a \cdot \max M + b \cdot \min M}{W} = \dots$$

$$\text{p. 366, eq. (8): } M = \max M + \frac{1}{2} (\dots)$$

## III a 2 M. Roš.

p. 411, eq. (7):  $\sigma_g = \sqrt{\dots + \gamma \tau^2} \leq \sigma_{o\ zul}$

p. 412/13: In the article "Obliquely placed fillet-weld"  
Accordingly we receive

$$\begin{aligned}\sigma_h &= \frac{P}{h}; \quad \sigma_1 = 0.25 \sigma_h; \quad \sigma_2 = 0.75 \sigma_h; \quad \tau = 0.433 \sigma_h \\ a_1 &= 0.35; \quad a_2 = 0.85\end{aligned}$$

$h$  = depth of weld

From the equation (6) — Fig. 20 — follows that

$$\begin{aligned}\sigma_h \cdot \sqrt{\left(\frac{0.75}{0.85}\right)^2 + 6 \cdot 0.433^2} &= 1.38 \sigma_h \leq \sigma_{o\ zul} \\ \sigma_h &\leq 0.72 \sigma_{o\ zul}\end{aligned}$$

## III c 1 N. C. Kist.

p. 518, 3<sup>rd</sup> li from the bottom:

$$\frac{1}{2} F \sigma_{B\alpha} = \frac{\sigma_B \text{ zug}}{\sqrt{\sin^2 \alpha + 3 \cos^2 \alpha}}$$

## IV a 3 H. Granholm.

p. 710, eq. (4a):  $(\dots) + e^{kx} (C \cos kx + D \sin kx)$

## IV b 1 S. Boussiron.

$$\text{p. 740: } J' = \frac{J_{crown}}{1 - \frac{K-1}{K} m^\gamma}$$

## IV b 2 Fr. Dischinger.

p. 761, 11<sup>th</sup> and 16<sup>th</sup> 1.: lowering of the crown of  $\frac{1}{3500} \frac{1}{2f}$

p. 769, 18<sup>th</sup> 1. from the bottom: .... 45,200 tm ....

## IV b 3 A. Hawranek.

p. 791, eq. (3): .... +  $\frac{1}{EF_m} \int \frac{N_x^2 ds}{A' + B'x + Dx^2}$

p. 792, 3<sup>rd</sup> 1.:  $\frac{H\Phi}{EF_m} \cdot \frac{2l\nu}{\varepsilon^2} \left[ \left( a + \frac{1}{2} \right) \ln \frac{\nu}{\nu_1} + \dots \right]$

## V 3 F. and H. Bleich.

p. 878, last equation: .... +  $\frac{1}{G} \sum_i \frac{T'_i h_i}{\delta_i} = 0$

p. 889, eq. (42), 3<sup>rd</sup> eq.: .... +  $EB_\varphi \frac{d^4 \varphi}{dz^4} - GJ_d \frac{d^2 \varphi}{dz^2} = 0$

## V 10 Fr. Krabbe.

p. 1032, 8<sup>th</sup> 1. from the bottom:

$$\dots - \frac{4E(J_{dm} + J_{d(m+1)})}{a} - \frac{6EJ_v}{h}$$

p. 1032, 4<sup>th</sup> 1. from the bottom:

$$\dots + J_{o(m+1)} \vartheta_{(m+1)} - 4J_{dm} \cos \alpha \frac{\vartheta_m}{2} \dots$$

p. 1033, 14<sup>th</sup> 1.:

$$= \frac{E}{a} \left[ -J_{o(m+1)} \vartheta_{m+1} + 4J_{d(m+1)} \cos \alpha \frac{\vartheta_{m+1}}{2} \dots \right]$$

p. 1034, eq. (30):  $M_m = -\frac{4EJ_o}{a}$

## V 11 B. Laffaille.

p. 1061, 10<sup>th</sup> 1.:  $\frac{d}{dr}(r z' \sigma_r) = Z r$

p. 1062, 3<sup>rd</sup> 1. from the bottom:  $\tau_{rs} = \sum t_n \cos n\vartheta$

## VI 1 Zd. Bazant.

p. 1098, eq. (15a):  $\omega' = \frac{1 - \cos \alpha}{\vartheta'} \left[ \dots \right]$

p. 1101, eq. (25a):  $y = \omega_0 r_0 \left[ \varepsilon - \delta \varepsilon + \frac{(p + p') r_2}{Et} \right]$

## VIII 1 A. E. Bretting.

p. 1491, last line:  $G = K \left( \frac{y}{10} \right)^n$

p. 1495, 21<sup>st</sup> 1.:  $c = 0.5 d$

p. 1497, 10<sup>st</sup> 1. from the bottom:  $G = K \cdot \left( \frac{y}{10} \right)^n$